



Spinning Fluids Reactor

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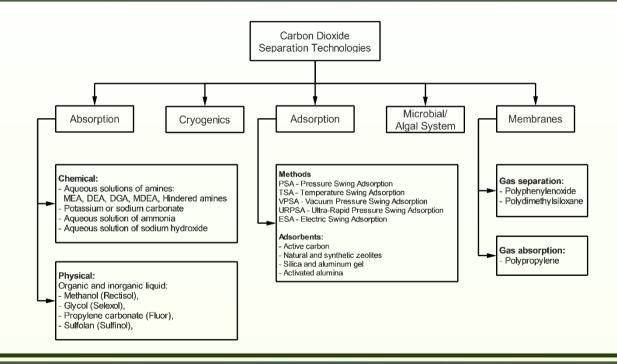


Outline of presentation

- 1. Introduction
- 2. Principle of design and operation of SFR
- 3. Flow hydrodynamics in SFR
- 4. Time of the hydraulic retention time in SFR
- 5. Interfacial area generated in SFR
- 6. SFR for biogas upgrading



Introduction Biogas valorisation methods





Introduction

Gas absorption equipment

- The liquid is dispersed in the form of droplets or discontinuous films in a continuous gas phase:
 - Spray tower
 - Packed tower
 - Venturi scrubber
- The gas is dispersed in liquid in form of bubble:
 - Mechanically agitated vessel
 - Tray Column
 - Bubble Column
- Both gas and liquid phases are continuous (for example, "a falling film contactor" which is used for gas-liquid reactions)



Introduction Gas absorption equipment

The main parameters affecting the gas absorption are:

- Resistance to gas flow
- Gas-liquid interface
- Liquid to gas ratios
- Liquid hold-up
- Flexibility to change gas and liquid phase flow
- Operating temperature range

Intensification of the mass transfer in absorption can be achieved by increasing:

- Gas-liquid interfacial area
- Increased mass transfer coefficient





Introduction

Mechanism of bubble generation in stagnant liquid

$$\overrightarrow{F_{\delta}} = \overrightarrow{F_{b}}$$

$$2\pi r_{k} \sigma = \frac{\pi d_{p}^{3}}{6} (\rho_{l} - \rho_{g}) N_{g} g$$

$$d_{p} = \sqrt[3]{12 \frac{r_{k} \sigma}{(\rho_{l} - \rho_{g}) N_{g} g}}$$

where:

 F_{σ} - surface tension force,

F_b - buoyant force,

rk - capillary radius,

 σ - surface tension of liquid,

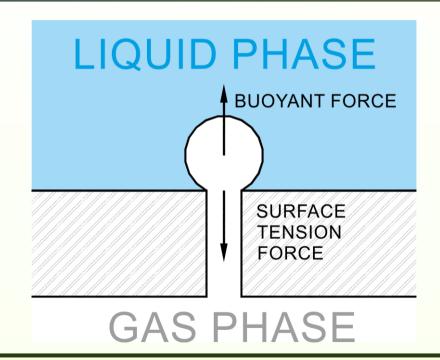
d_b - bubble diameter at laminar flow,

 ρ_{l} - liquid density,

 ρ_a - gas density,

N_q - dimensionless centripetal acceleration,

q - gravity acceleration





Introduction

Mechanism of bubble generation in flow liquid

$$\overrightarrow{F_{\delta}} = \overrightarrow{F_{w}} + \overrightarrow{F_{s}}$$

$$\overrightarrow{F_{s}} = \xi \frac{\rho_{l} u^{2}}{2} \frac{\pi d_{b}^{2}}{4}$$

$$2\pi r_{k} \sigma = \frac{\pi d_{p}^{3}}{6} (\rho_{l} - \rho_{g}) N_{g} g$$

Laminar flow

Turbulent flow

$$d_l = \sqrt[2]{\frac{16r_k\sigma}{\xi\rho_l u^2}}$$

$$d_t = \frac{1}{4} \sqrt[4]{\frac{r_k \sigma \eta^2}{f^2 \xi \rho_l^3}}$$

where:

 \boldsymbol{F}_{σ} - surface tension force,

F_b - buoyant force,

rk - capillary radius,

 σ - surface tension of liquid,

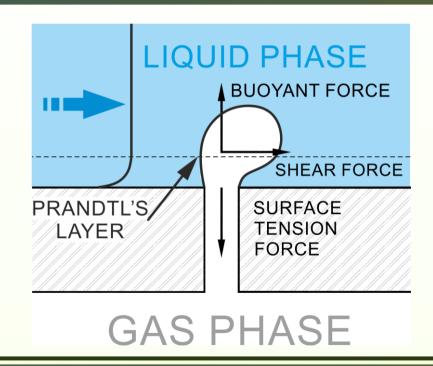
d_b - bubble diameter at laminar flow,

 ρ_l - liquid density,

 ρ_0 - gas density,

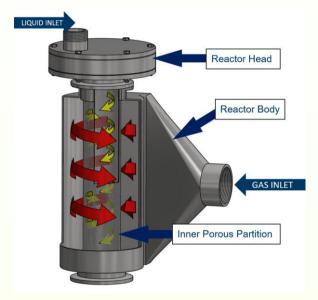
N_a - dimensionless centripetal acceleration,

q - gravity acceleration





Principles of Spinning Fluids Reactor operation





CFD simulation of gas-liquid interface formation in SFR. Performed by Krzysztof Tesch.

J.D. Miller, J. Hupka, and R. Aranowski, Spinning fluids reactor, 2012, Patent US 20110223091 A1; WO 2010014918 A3



Pressure drop during gas flows through a liquid layer

$$\delta P_L = \int_{R-\delta}^R \rho_L \frac{u_t^2(r)}{R} dr$$

where:

 u_t - tangential velocity,

R - radius of the porous partition,

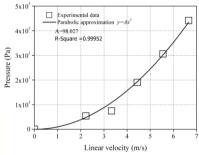
r - radius,

 δ - thickness of the spinning liquid layer

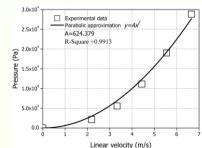
 ρ_1 - liquid density

$$P_c \propto u_t^2$$

Type of porous partition	The thickness of the spinning liquid layer (mm)	
Cylindrical	2.5	
Conical (1.5°)	8.0	
Conical (3.0°)	11.6	



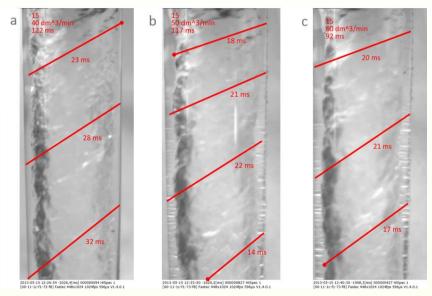
Pressure exerted on the inner wall of the cylindrical porous partition by the spinning liquid layer vs. Linear inlet velocity $\,$



Pressure exerted on the inner wall of the conical porous partition (3.0°) by the spinning liquid layer vs. linear inlet velocity



Optical measurement of the hydraulic retention time in SFR

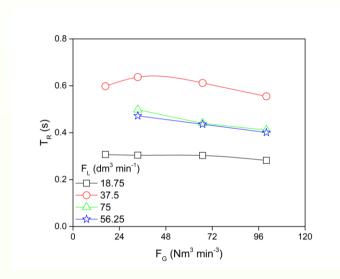


Trajectory of the liquid streamline in SFR for varied inlet velocities: a) 4.40 m·s-1, b) 5.51 m·s-1, c) 6.61 m·s-1

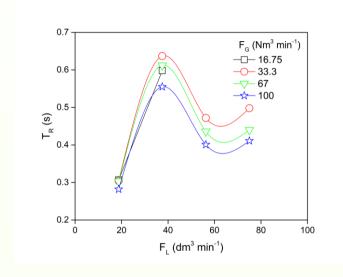
The hydraulic retention time in SFR is in the range of 0.09-0.3 s



Hydraulic retention time



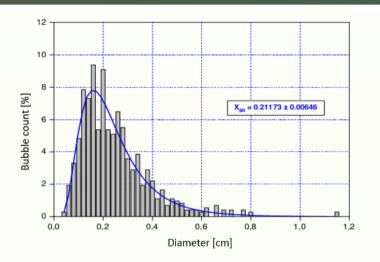
Hydraulic retention time vs. flow rate of the gas phase



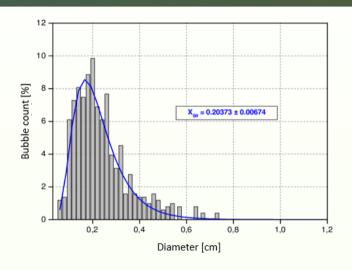
Hydraulic retention time vs. flow rate of the liquid



Size Distribution of Gas Bubbles Generated in the SFR



 $Q_W = 20 \text{ dm}^3 \cdot \text{min}^{-1}, Q_G = 25 \text{ m}^3 \cdot \text{h}^{-1}$

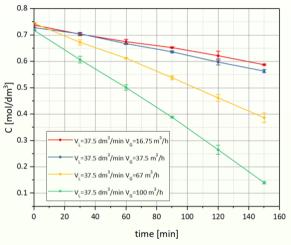


 $Q_W = 20 \text{ dm}^3 \cdot \text{min}^{-1}, Q_G = 55 \text{ m}^3 \cdot \text{h}^{-1}$

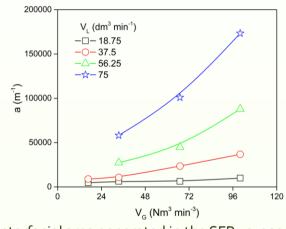
Aranowski R, Wojewódka P, Zielińska-Jurek A, Bokotko R, Aranowski R, Wojewódka P, et al. Spinning Fluids Reactor: A new design of a gas – liquid contactor. Chem Eng Process Process Intensif 2017;116:40–7. https://doi.org/10.1016/j.cep.2017.03.005.



Interfacial area generated in the SFR



Change in sulphite concentration vs. aeration time



Interfacial area generated in the SFR vs. gas phase flow



Perforated metal sheet Rv1-2 with round meshes (d=1 mm) was used as porous partition.

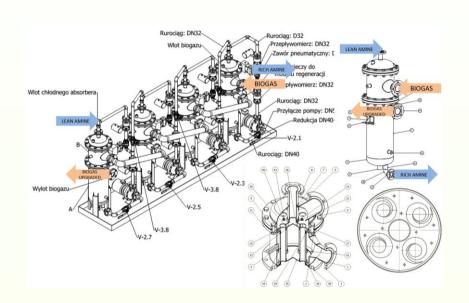


Comparison of interfacial area and mass transfer coefficient of SFR with various absorption equipment

Absorption equipment	a [m²/m³]	k _{La} ·10² [s ⁻¹]
Packed Columns (countercurrent)	10-350	0.04-7
Packed Columns (co-current)	10-1700	0.04-100
Sieve plate Columns	100-200	1-40
Bubbling Columns	50-600	0.5-24
Packed Bubbling Columns	50-300	0.5-12
Scrubbers	10-100	0.07-1.5
Stirred Tank Reactors	210-450	12.5-29.1
Jet reactor	1000-7000	0.1-3.0
Venturi Reactor	160-2500	8-25
Cyclone Centrifugal Bubbling Reactor	1000	-
Airlift Multistage Reactor	70-300	1-5
SFR	2190-162800	74.8-5935



Confirmation of SFR effectiveness







Directions of investigation in the LoCaGas project

Absorbent selection and development:

Aassumptions:

- Desorption at low temperatures (80–90°C)
- Low capital expenditure (CAPEX)
- Fast CO₂ absorption kinetics
- High resistance to oxidation and degradation

Optimization of SFR design and operating parameters:

- Enhance contact time and interfacial area by optimizing the design of dispersive structures.
- Optimize rotational speed and flow rate to enhance mass transfer
- Validate performance under realistic capture and desorption conditions



Conclusion

- SFR is an extremely effective device for contacting the gas and liquid phases.
- Due to the short retention time, the SFR should be used in processes with fast kinetics.
- The gas phase pressure drop in the SFR does not exceed a few kilopascals.
- SFR system can be used for biogas upgrading for small and medium flow rate of raw biogas (up to several hundred m³h⁻¹).
- Due to its small size of SFR, it can be built in a container system.
- SFR has a simple design that guarantees reliable operation





THANK YOU FOR ATTENTION

Do you have any question?

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